CATAWBA NUCLEAR STATION
UNIT 2
EVALUATION OF 2EOC13 ISI
FLAW IN SG2C TO HOT LEG WELD
CNC-2201.01-00-0006

Form 101.1 (R08-04)

	CERTIFICATION	OF ENGINEERIN	NG CALCULAT	ION										
Station And Unit Number	Catawba Nucl	ear Station, Unit 2	2											
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Statement of Problem / Purpose

This calculation has been performed to address an indication discovered on the 2C Steam Generator to Hot Leg weld during 2EOC13. This particular weld is located between the cast low alloy steel primary channel head of the steam generator and the cast austenitic stainless steel elbow. Typically, the volumetric examination under Section XI of the ASME Code would be performed using an ultrasonic examination. However, the cast austenitic stainless steel material of the reactor coolant loop piping precludes the use of the ultrasonic examination methodology. The ultrasonic examination was replaced with a radiographic examination.

QA Condition

This calculation is QA Condition 1 because it serves as the basis for continued qualification of a Duke Class A, ASME Class 1 component.

Analysis Methodology

This calculation verifies that the structural integrity of the steam generator 2C nozzle to hot leg weld is maintained under all operating and design loading conditions, even with the identified flaw. The verification has been performed by conservatively bounding the flaw characteristics and comparing this bounding flaw against allowable flaw depths provided by a Westinghouse flaw evaluation handbook [7] specific to this reactor coolant loop location.

Other Evaluation Criteria

No other evaluation criteria have been used.

Applicable Licensing References

- L. 1 Catawba UFSAR, September 27, 2003 issue date, Sections 3.9 and 5.2
- L. 2 Catawba Selected Licensee Commitments 16.5.5, Reactor Coolant System, Structural Integrity, Rev 0

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Assumptions/Engineering Judgments

As noted in body of calculation

Catawba Nuclear Station, Unit 2 Evaluation of 2EOC13 ISI Flaw in SG2C to Hot Leg Weld CNC-2206.01-00-0006, Rev. 0

References

- 1 ASME Code, Section III, Subsections NB and NC, 1974 Edition with Summer 1974 Addenda.
- 2 ASME Code, Section XI, 1989 Edition, No addenda
- Westinghouse sketch EDSK 380335B, from CNM-2201.01-0217
- 4 Westinghouse sketch EDSK 380329B, from CNM-2201.01-0217
- 5 CNM-1201.01-0076, Rev 0, ESCO drawing AA-43234, , Weld Bevel Detail, 31.00 I. D. Elbows, Nozzle Ends
- 6 CNM-2201.01-0008, Rev B, ESCO drawing AD-22321, Machining 31.00 I.D. x 29.00 I.D. Long Radius 50° Reducing Weld Elbow
- WCAP-15658-P, September, 2004, Flaw Evaluation Handbook for Catawba Unit 2 Steam Generator Primary Nozzle Weld Regions.
- 8 CN-2553-1.0, Rev 22, NC Flow Diagram.
- 9 CN-2NC-0013, Rev 13, Weld Isometric.
- 10 PIP C-04-5421

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Calculation/Evaluation

This calculation was performed by determining the bounding characteristics of the indication and comparing parameters associated with this indication to values in the Westinghouse supplied flaw analysis handbook [7].

Nozzle Configuration

The nozzle connection consists of a low alloy steel casting that forms the channel head of the steam generator. This casting has been buttered with a low carbon, stainless steel weld metal. The piping to buttering field weld is made after post weld heat treatment of the steam generator channel head. The Duke weld number is 2NC-13-2 and the weld process control from the original fabrication is included as Attachment A. This weld is a full penetration, compound V groove weld made from the outside of the pipe. The GTAW (TIG) process was used for the first inch, followed by a "courtesy" radiograph (RT). Subsequent welding was performed using the SMAW (stick) process to finish out the weld. After completion of welding, a final RT was performed and accepted on the weld. In addition, liquid penetrant tests (PT's) were performed on the interior and exterior surfaces of the weld.

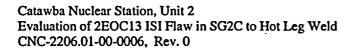
Flaw Geometry

The flaw is located at the bottom of the pipe in the C hot leg. It is approximately at bottom dead center of the pipe. Based on the radiographic data, the flaw is 1" long and oriented in the circumferential direction. Since the examination was performed using RT, a limited amount of information was available to characterize the flaw. The location of the flaw relative to the OD surface was established using parallax radiographic shots. These shots support a minimal flaw depth. However, because of the uncertainty in flaw depth, a bounding case has been reviewed herein.

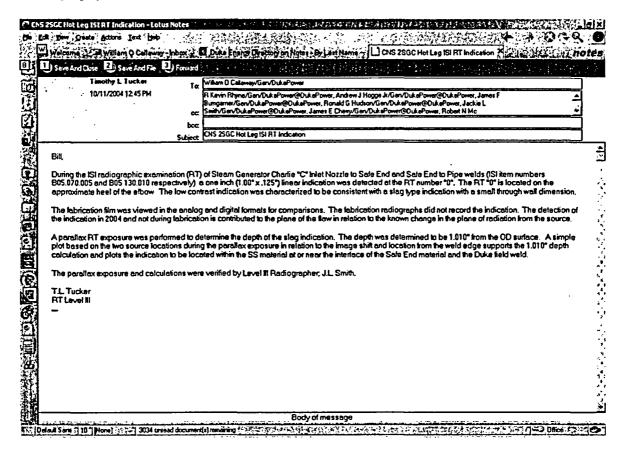
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Radiography Evaluation



In addition to the radiography shots made to characterize the flaw, both the original construction film and the 2EOC13 film (non-parallax shots) were digitized. The original construction film was digitized to determine if the indication could be seen from initial fabrication welding. Digitization of the film can greatly enhance the visible interpretation of the film in some cases. Next, the 2EOC13 film was digitized and reviewed to determine if the linear indication was actually separated into multiple flaws. In both of these cases, there was no conclusive evidence from the digitization process that changed the film interpretation or flaw characteristics.

Based on the conclusions provided from the radiography review above, a best estimate characterization of the flaw has been provided. The flaw is located 1.01" from the outside surface of the piping in the stainless steel weld material. The flaw is oriented circumferentially with a length of 1.0". The flaw is most likely the result of a slag inclusion during fabrication. It has very little contrast that indicates a limited depth. It is located at the interface between the stainless steel buttering and the Duke stainless steel field weld.

The flaw location from the OD surface of 1.01" was considered from three positions relative to the flaw depth (top, center & bottom). The three positions were considered for two different aspect ratios. All six cases were found to be acceptable. Based on the method used to determine location, the center position is the most appropriate and is used in the documented flaw calculation below.

For the initial evaluation, the flaw depth will be assumed as ½ of the length and evaluated as an embedded flaw. From the flaw handbook, several parameters are necessary to determine the acceptability of the indication. These are provided below. The appropriate figure for the purposes of evaluation from reference [7] for a circumferential embedded flaw in the stainless steel material is Figure A-3.7.

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a = half flaw depth (in)
= 0.25 in.
l = length of flaw (in)
= 1.0 in.
t = wall thickness (in)
= 3.25 in.
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Note: The wall thickness is based on profiling of weld using UT probe. Value of 3.25" is conservative and represents the lowest reading throughout the weld region of interest. See page for the UT profile readings at the location of interest.

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\delta = distance to flaw centerline
= 1.01 in.
\delta/t = 1.01 / 3.25
= 0.311
a/t = 0.25 / 3.25
= 0.077
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The δ / t and a / t parameters may be plotted on Figure A-3.7 to determine the acceptability of the flaw. This point (A) is shown on the attached sketch.

In addition to the above evaluation, the flaw depth was increased to 1" yielding an aspect ratio of 1:1. In this case, the parameters change as noted below:

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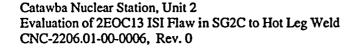
Page 5

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a = half flaw depth (in)
= 0.50 in.

l = length of flaw (in)
= 1.0 in.

t = wall thickness (in)
= 3.25 in.

δ = distance to flaw centerline
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= 1.01 in. $\delta/t =$ 1.01 / 3.25 = 0.311 a/t = 0.50 / 3.25 = 0.154

Again, the δ / t and a / t parameters have been plotted on Figure A-3.7 as point (B) to determine the acceptability of the flaw.

Results

In both cases evaluated above, it is clearly evident that the flaw is within the bounds of the acceptability provided by Figure A-3.7 of reference [7]. As a result, the piping containing this flaw is acceptable for continued service for the design life of the plant. The figure in reference [7] indicates 10, 20 and 30 year acceptance lines. These lines are related to the design number of occurrences of transients used in the fatigue crack growth calculation. As such, this indication is acceptable for life of plant provided a prorated value (30/40 = 75%) of the design number of occurrences are not exceeded between now and end of plant life. This limit on fatigue cycle counts will be tracked under our fatigue management program.

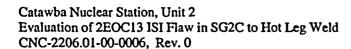
Conclusion

The flaw discovered during 2EOC13 is acceptable without repair for the life of plant. Acceptance by the performance of analytical evaluation as allowed by ASME XI, IWB-3132.4 has been validated. Additional examinations have been performed during 2EOC13 to satisfy IWB-2430. Successive examinations for the SG2C hot leg weld number 2NC-13-2 will be necessary in the subsequent three ISI periods as required by IWB-2420.

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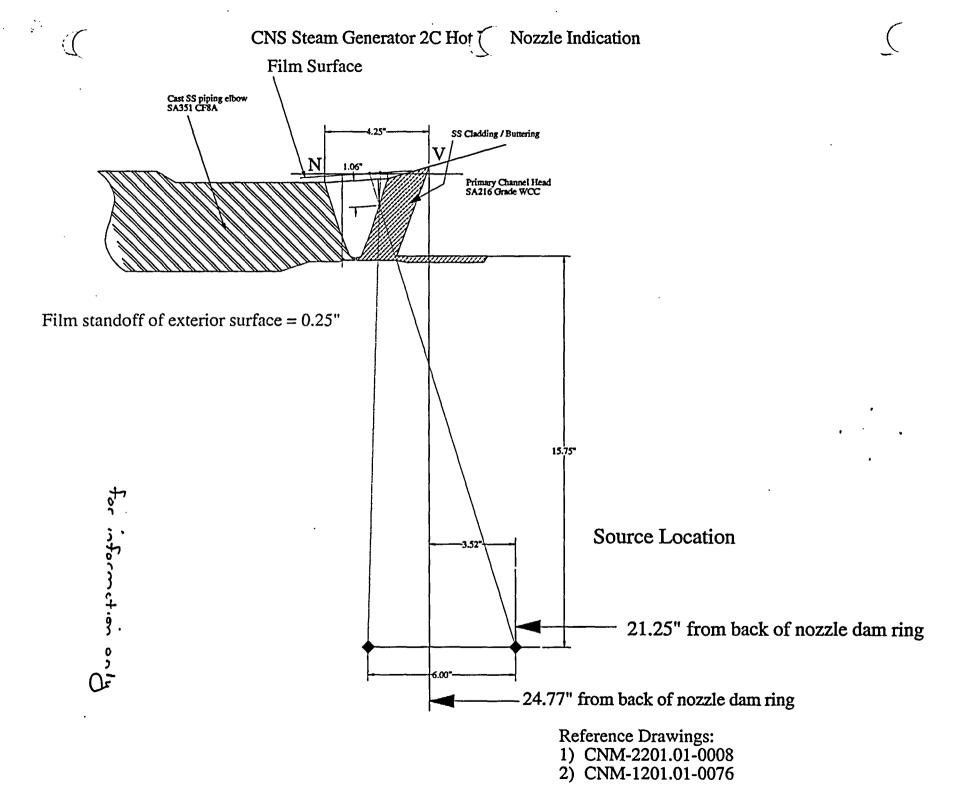
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Page 7 Proprietary

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TINU.		YSTEM_		·	Y/DRAWING NO. CN-		WFLU 1:0	2N.4.	/3. - 2
Postio ha	NELS! *		ture.	TTPE	HCTL/FOL	THE PARTS	3276	43175*54	24
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	FKII	406		l	·	1.304.11	12.19.30	TUT	1.8
	FRH	1106	3/32	2 508.16	8686€	1.30411	12.19.80	TOUT.	:. <u> </u>
	LLB.	X89	3/32	£329=16.		\L:\$&Y:4L.	7.12.12	Kurk	1.8
0_	RLB_	X89	1/4	E308:16			12:15:80	Kure	1.5
	FKH	HOL	18	230816	8665	2.304.11	1278.80		ŗ
0	FKH	1106	3/3/2	230816	Si YOE	2 304.11	02-נת בנ	KWK	1-8
0	RRB	X.89	732	E 308-16	8680E	4304-11	12-19-50	KWK	1.8
0	RRB	X59_	1/8	£308-16	8665	1304-11	12-19:80	Kuf	1.8
	RRB.	189	1/5	£ 308-16	_8665	1 -	12:22.8	. Kuf	1.8
	ORB	X81	7/57	E305-16	8680E	1304-11	12.22.50	. pull	1-8
	FKH	AO b	3/32		अ८४० ह		1.3-12.80		1.8
0	FRII	HOL	1/3'	2 05 16	846.5	-32411	12230	Kwk	1.8-
اء	FKH	HOL	4	2: 7.76	J. L. 5	- Sey 11	نويدي	KWK	1.8.
3	FRH	HOL	1	٠٠ ٧٠٠ ج	16.10€	37411	٥٤٠ وحدد.	Kurk	1.8.
1)	RRB	X89	732	£ 308-16	8680E	4.34.11	12 22:80	KwK	1.8
	RRB	X89_		F.308-16.	3665		12.22.50	KWK	1.8
	RRB	X89.	18	EZS://:	8665		12.29.50		1-8-
	RRB	184	332	£308:16	8480.E	4.304-11	12.29.50	Kive	1-8
0	FRH	406	1/2	301.6	y 2 80 E	1. 3.4.11	1 11	Kwk	1.8
-0	FKI	1106	11	131116	12 6.5	. 184-11	12.20.50	Ku K	1-8
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Ò	FRH	106	3/22	3887	3.506	£ 304-11	12.27 80	KWK	1-8-
	REB		¥32	E.308-16	8680E	4.304-11	12-29:80	LWK	1.8-
	ers.		1-4	E 308:14	8465	1300-11	12.79.50	KuK	1.8
	RRB	X89_	18	£309-14	5685	L 304-11	12-30-80	KwK	1.3.
	RRB		7,2	E.305-16	_\$680E	43/4-11	12.30 50	Kert	1.8
0	FKF	466	3/52	203.00	, , , , , e	2.334.11		KwK	1-8-
	FXH	706	41	23.00	8005	: 334.11	10 10	KwK	18
· ·	RRB	ļ·	15	E 308-16			12.30.80	Kisk	1.0.
	RRB	189	1	ESCY:16			12.8560	11 77 2	18
; ! e :- ·		···s c··				<u>. 29211</u> 2	72.13 <u>9.6.1</u>		, <i>K</i>

Attack A P3 6 Cuc. 2801.01-00-0006

D FRH HOL YS E308-16 8665 C308-11 12-30-80 KWK 1- D FRH HOL YS E308-16 4680 C50411 12-31-80 KWK 1- D FRH HOL YS E308-16 4680 L-50411 12-31-80 KWK 1- D FRH HOL YS E308-16 3665 L-50411 12-31-80 KWK 1-		マンンも9 11/21。	/79			TU1.15	14-4L	EVISIG	4:	1
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D FKH HOL 3/2 E308.16 .96.80E 2.504.11 .2.30.90 KwK 1. D FKH HOL 1/2 E308.16 96.80E 1.304.11 .2.31.80 KwK .2.308.11 .2.308.11 .2.308.11 .2.308.11 .2.308.11 .2.308.11 .2.308.11 .2.308.11 .2.308.11 .2.308.11 .2.308.11 .2.308.11 .2.308.11 .2.308.11 .2.308.11 .2.308.11 <td< td=""><td>log as low</td><td>CHIEC.</td><td>STETCH. HUVYEH</td><td></td><td>1447</td><td></td><td>1:212 2:45:</td><td>37.10</td><td>-1-1-6-6-</td><td>,</td></td<>	log as low	CHIEC.	STETCH. HUVYEH		1447		1:212 2:45:	37.10	-1-1-6-6-	,
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0 FRH HOL 28 E3CX-16 :: 65 2-364-11 12-31-80 KWK 1-	7			1/32	E 30816	46.905	2.30411	12.31.50	KWK	1-2
D RRB X89 1/8 E 308:16 81:65 1 304-11 12-31-80 MwK 1-			136	23	E308-16	7665	2-304-4	12.31.80	Kuk,	1.2
	2			18	£308:16		_1.304-11.	12-31-80	KuK	1-2
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Attent A, PS 7 CNC-2201.01-00-0006

PIP Serial No:	Action Category: Action
C-04-05421	3

Problem Identification

Discovered Time/Date:

10:33 10/11/2004

Occurred Time/Date:

10/07/2004

Unit(s) Affected:

<u>Unit</u>

Mode %Power Unit Status Remarks

2

NOMODE

System(s) Affected:

NC

Reactor Coolant

Affected Equipment

(No Equipment Affected)

Location of Problem:

Bldg: RX

Column Line:

Elev:

Location Remarks:

S/G 'C'

Method Used to Discover Problem:

RT (ISI) of S/G'C' Inlet/outlet nozzle weld

rief Problem Description:

mear indication of I inch found in S/G 'C' on Hot leg during RT(radiography)

Detail Problem Description:

Linear indication of 1 inch found in S/G 'C" hot leg nozzle weld duirng RT.Linear indication of 1 inch exceeds the acceptance standards of NDE-12, ASME Code Sections III and XI.(Procedure NDE 12 Rev. 11, Appendix A, ASME Code XI IWB-3514, ASME Code Section III NB-5320). Slag indication of 1 inch in length located at RT film interval number '0'. The indication was not visible on the construction radiographs. A change in the source position in relation to the plane of the flaw was determined to be the basis for the flaw detection in 2004 and not during the fabrication RT. This is a reportable indication.

Originated By: JFB8158: BUMGARNER, JAMES F Team: JLW3805 Group: IWS Date: 10/11/2004

Other Units/Components/Systems/Areas Affected(Y,N,U): U

Industry Plants Affected(Y,N,U):_U

Immediate Corrective Actions:

Engineering to perform Fracture Mechanics Analysis.

Originated By: JFB8158: BUMGARNER, JAMES F Team: JLW3805 Group: IWS Date: 10/11/2004

Immediate Corrective Action Documents / Work Orders:

Screening

Action Category: 3 Root Cause performed? No

10/11/2004 11:33 Page 1 PIP No: C-04-05421

	ĴγEP No:				
	Other Report Nos:				
	Event Codes: F8 Testing				
	Screening Remarks:				
	Originated By: MLS9465: STANDRIDGE, N	AICKEY L Team: PA	AM7334 Group: S	SRG Date: 10/11/20	04
	Assignments: Responsible Groups(s) for Problem Evaluation Responsible Group for Present Operability: Responsible Group for Report Support Info:	N/A N/A	Mechanical/Ci	vil Eng	
	Responsible Group for Reportability: Responsible Group for Overall PIP Approval	N/A : IWS	INSPEC. & W	ELD. SERV.	
	Signature Type Greened By: MLS9465	Team PAM		Group SRG	10/11/2004
1	Present Operability				
	kesponsible Group:	Status:			
	Sys/Comp Operable? (Y.N,C,E,T):				
	Required Mode:				
	Comments:				
	No Current Signatures 1	For This Section			
	<u>Reportability</u>				
	Responsible Group:	Status:			
	Problem Reportable(Y,N,E):				
	Reportable Per:				
	Comments:				
	No Current Signatures 1	For This Section			
	Investigation Report:				
	esponsible Group:	Act Date:			
	avestigator: Group	p: _.			
	Due Date:				
	10/11/2004 11:33		Page 2		PIP No: C-04-0542

Date Due to VP or Sta. Mgr:

Pate Regulatory or Agency Rpt Due:
Date Investigation Report Approved:

NRC Cause Codes:

Report Support Info:

Responsible Group:

Status:

No Current Signatures For This Section

Problem Evaluation



Problem Evaluation From: Resp. Group: MCE

Status: ReadyForAccept

OEDB Checked: No

OEDB Comments:

Remarks Comments:

/ <u></u>			
Signature Type	Indiv	Team Group	Date
Assigned To:		MCE	10/11/2004
Due Date:	11/10/2004		

Corrective Actions

CA Seq. No: 1

-					
Free Street Control	CAR COLL SALVEST	A STATE OF THE PROPERTY OF THE PARTY OF THE	CONTRACTOR OF A STATE OF THE	THE RESERVE OF THE PARTY OF THE	Cause Code
L Resp Ciroup	Central Status Level	Distriction of the control of the co	- In Fight Went Gode	TAKE PRODUCATOR	* E Cause Code * * * * * * * * * * * * * * * * * * *
1232 P1 - 1 - P	Cattle to a second by the ball	11. C.		24	
RGC	Onen	111/0	Eō	۸.7	vvv i
INGC	Open	1142	1.0	7.4	111

Proposed Corrective Action:

Notify the NRC of the Reportable indication.

Originated By: JFB8158: BUMGARNER, JAMES F Team: JLW3805 Group: IWS Date: 10/11/2004 No Current Signatures For This Section

General:Outage:

Mode:

Other Tracking Processes

Type Number Text

Actual Corrective Action:

Priority: N

Actual CAC:

Status:

Due Date:

-Signature Type	Indiv : 11	Team and the	Group	Date Land State Control
Assigned To:			RGC	10/11/2004

CA Seq. No: 2

Resp Group	Status	Orig Group	🛂 💤 Event Code	Prop CAC	Cause Code
RGC	Open	IWS	F8	A2	YYY

Proposed Corrective Action:

Provide Fracture Mechanics Analysis data to the NRC for their review prior to unit re-start.

Originated By: JFB8158: BUMGARNER, JAMES F Team: JLW3805 Group: IWS Date: 10/11/2004

No Current Signatures For This Section

General: Outage:

Mode:

Other Tracking Processes Number Text **Type**

Actual Corrective Action: Priority: N

Actual CAC:

Status:

Due Date:

Signature Type	Indivities Team To The Art The Group	Date The State of the State of
Assigned To:	RGC	10/11/2004

Final and Overall PIP Approval

Responsible Group: IWS

Status: Screened

Signature Type	Group (%)	Print Date in the	以
Assigned To:	IWS	10/11/2004	

Any Supplemental Concurrence Signatures Above Do Not Affect PIP Closure.

Closure Document Type

Closure Document No

Attachments

Generic Applicability

Responsible Group:

Status:

GO PIP No:

Assessment Remarks:

No Current Signatures For This Section

Failure Prevention Investigation

No FPI Records for this PIP.

ار	Re	m	ar	ks

No Remarks for this PIP.

Maintenance Rule No Maintenance Rule Records for this PIP.

End of the Document for PIP No:

C-4-5421

The status of this PIP is:

Screened

The duration of this PIP was:

0 days



		<u> </u>			1 WA-310	A Revision 4			
	Indication Evaluation Report								
	STATION Catawba	UNIT 2		ITEM NUM .070.005 .130.010		ISI PLAN ID NUMBER 2SGC-INLET-SE 2NC13-02			
	NDE METHOD Radiography		NDE PROCEDURE USED NDE 12 REV. 11			INDICATION SERIAL NUMBER S/N 1 (located at RT # 0)			
	DESCRIPTION OF Steam Gen Ini Steam Gen No	et Nozzle to S	Safe End Weld		SPECTED 7/2004	EVALUATION NEEDED BY DATE 10/11/2004			
A	indication was n	ot visible on lane of the fla	the construction r	adiograp	hs. A cha	erval number "0". The nge in source position in e flaw detection in 2004 and not			
	ORIGINATED BY	': T.L. Tucker		•	DATE: 1	0/11/2004			
	ACCEPTANCE S IWB-3514, ASME			DE 12 Re	v 11 Appei	ndix A, ASME Code Sect. XI			
В	CALCULATIONS of NDE 12, ASME			length of	f 1.00" exc	eeds the acceptance standards			
	EVALUATION STATUS = Reportable								
	Evaluated By (NDE LEVEL III):	T.L. Tucker			DATE: 1	0/11/2004			
С	PIP SERIAL No:	C-04-54	21						
<u> </u>	ISI COORDINATO	DR:		DATE:					
	ADDITIONAL INSPECTIONS . NOT REQUIRED REQUIRED: ISI PLAN ADDENDA S/N:				A S/N:				
D SURVEILLANCE INSPECTIONS NOT REQUIRED REQUIRED: ISI PLAN ADDENDA S/N:				A S/N:					
	ISI PLAN MANAGER DATE								
Ш		DISPOSITION ACCEPTABLE IN ACCORDANCE WITH IWB-3600 (FMA) REPAIRED REPLACED							
	DISPOSITIONED	BY (ISI Plan M	fanager)			DATE			

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